

REMARKS

In the Office Action of March 25, 2003, the finality of the Office Action of June, 27, 2002 was withdrawn in light of Applicants' request for continued examination. In addition, the Office Action found a lack of unity of invention and, thus, required election of a single invention from Groups I – IV, as identified.

Applicants' request reconsideration of the finding of a lack of unity of invention in view of the following arguments. In the event that the arguments presented are not found to be persuasive, Applicants' provisionally elect, with traverse, the claims identified in Group I for examination.

Election / Restriction

The Office Action of March 25, 2003 separated the pending claims into four groups of inventions (Groups I-IV), which allegedly "are not so linked as to form a single general inventive concept under PCT Rule 13.1" because "under PCT Rule 13.2, they lack the same or corresponding special technical features." While the Examiner acknowledged that the inventions of groups I-IV "all relate to a detectable reagent comprising discrete particle dispersed in a carrier, diluent, excipient, adjuvant, wherein said particle comprises a detectable marker encased in at least two layers of carbon," she concluded that "the technical feature linking the inventions of groups I-IV does not constitute a special technical feature as defined by PCT rule 13.2, as it does not define a contribution over the prior art." In support of this assertion, the Examiner characterized the Burch *et al.* reference as teaching "Technegas (a plurality of discrete particles comprising a plurality of coating layers of carbon which completely enclose a minute crystal of ^{99m}Tc metal) in an aqueous aerosol."

The methods and reagents in pending claims 31 – 79 relate to stable diagnostic and therapeutic colloids for the selective detection of fibrin in aqueous environments. Applicants agree with the Examiner's assertion that the pending claims share a technical feature in common in that they each involve "a detectable reagent comprising discrete particle dispersed in a carrier,

diluent, excipient, adjuvant, wherein said particle comprises a detectable marker encased in at least two layers of carbon." Applicants emphasize, however, that colloids of the present invention comprise carbonaceous particles dispersed in an aqueous medium. The combination of (i) selective binding to fibrin and (ii) stable association with an aqueous media exhibited by the diagnostic and therapeutic particles of the present invention provide "a technical relationship . . . involving one or more of the same or corresponding technical features . . . that define a contribution which each of the claimed inventions, considered as a whole, makes over the prior art." Patent Cooperation Treaty, Rule 13.2.

As conceded by the Examiner, pending claims 31 – 79 have a technical feature in common, namely use of diagnostic or therapeutic carbonaceous particles dispersed in an aqueous medium for the detection of fibrin. Applicant submits that searching for prior art relevant to all the claims of Groups I - IV does not present a significant burden because the pending claims are linked by such a specific and well defined technical feature. It is further submitted that the Examiner's conclusions regarding the scope of the contribution of the present invention to the prior art are better evaluated in the context of 35 U.S.C. §§ 102 and 103 statutory requirements.

In addition, the acknowledged technical features common to pending claims 31 – 79 do represent inventive contributions over the prior art because no prior art reference or combination of references teach diagnostic or therapeutic carbonaceous particles dispersed in an aqueous medium for detecting fibrin. Contrary to the Examiner's characterization, Burch *et al.* (1986) does not teach a plurality of discrete particles comprising carbon layers enclosing a crystal of 99m TC metal dispersed in an aqueous aerosol. Rather, Burch *et al.*'s teaching is limited to the formation of a diagnostic colloid comprising discrete carbonaceous particles dispersed in a gaseous argon continuous phase. Indeed, the particle formation process described in Burch *et al.* involves "evaporation to dryness of 140 MBq of sodium pertechnetate" in a graphite crucible by heating the crucible "to 2500° C in an atmosphere of pure argon." (See, Burch *et al.*, pg. 866, lines 18-24, emphasis added). Assuming a constant heat of vaporization of water of 44.016 kJ/mol as a function of temperature and a vapor pressure of water at 374 ° C of 1.65×10^5 Torr, the vapor pressure of water at the synthesis temperature employed in Burch *et al.*, 2500 ° C, is predicted to be approximately 1.16×10^5 Atm. (see, Exhibit A, a table from the Handbook of

Chemistry and Physics, 67th Ed., showing the vapor pressure of water as a function of temperature a table from Physical Chemistry by P.W. Atkins, showing heats of vaporization and an estimate of the vapor pressure of water at 2500°C). Any water in the system described by Burch *et al.* is in the gaseous state during particle formation. Therefore, it is not physically possible for water in the described particle generation system to be available as an aqueous medium (a liquid) for the dispersion of carbonaceous particles.

Further, there is no suggestion in Burch *et al.* to modify the diagnostic particles described therein to provide carbonaceous particles dispersed in aqueous media. Rather, Burch *et al.* teaches away from the use of particles in aqueous media. For example, Burch *et al.* note on page 866, lines 4 - 10, that the "many limitations" associated with aqueous aerosols of technetium prompted their investigation of non-aqueous diagnostic particles. Moreover, the reference reports the benefits of non-aqueous radioactive tracers exhibiting no "clearance from the lungs" and having long diagnostic half-lives. As Burch *et al.* does not disclose or even suggest the existence of carbonaceous, fibrin-binding particles dispersed in an aqueous medium, it cannot be relied upon as disclosing the technical feature linking the claims of Groups I-IV.

In view of the foregoing, it is submitted that the lack of unity of invention is improper. Accordingly, reconsideration and withdrawal of the lack of unity of invention is respectfully requested.

Conclusion

Based on the foregoing, this case is considered to be in condition for allowance and passage to issuance is respectfully requested.

This Amendment is accompanied by a Petition for Extension of Time. Please deduct the fee of \$110.00 as required by 37 C.F.R. 1.17 from Deposit Account No. 07-1969. If this amount is incorrect, please deduct the appropriate fee for this submission from Deposit Account No. 07-1969.

If there are any outstanding issues related to patentability, the courtesy of a telephone interview is requested, and the Examiner is invited to call to arrange a mutually convenient time.

Respectfully submitted,



Donna M. Ferber
Reg. No. 33,878

Greenlee, Winner and Sullivan
5370 Manhattan Circle, Suite 201
Boulder, Colorado 80303
Phone: (303) 499-8080
FAX: (303) 499-8089
E-Mail: winner@greenwin.com
Attorney Docket No. 5-00
DMF:lla:4/29/2003

VAPOR PRESSURE OF WATER ABOVE 100°C (continued)

Temp. °C	Pressure		Temp. °F	Temp. °C	Pressure		Temp. °F	Temp. °C	Pressure		Temp. °F
	mm	Pounds per sq. in.			mm	Pounds per sq. in.			mm	Pounds per sq. in.	
208	13742.33	265.793	406.4	284	37529.56	725.703	507.2	320	84486.80	1637.575	606.0
209	14022.76	271.156	408.2	285	38133.00	737.372	509.0	321	85819.20	1659.472	609.8
210	14305.48	276.623	410.0	286	38742.52	749.138	510.8	322	86959.20	1681.316	611.6
211	14595.04	282.222	411.8	287	39361.92	761.135	512.6	323	88114.40	1703.854	613.4
212	14888.40	287.895	413.6	288	39986.66	773.215	514.4	324	89277.20	1726.339	615.2
213	15184.80	293.626	415.4	289	40619.72	785.477	516.2	325	90447.60	1748.971	617.0
214	15484.04	299.490	417.2	290	41261.16	797.861	518.0	326	91633.20	1771.897	618.8
215	15792.80	305.383	419.0	291	41910.20	810.411	519.8	327	92826.40	1794.969	620.6
216	16104.40	311.408	420.8	292	42566.08	823.094	521.6	328	94042.40	1818.487	622.4
217	16420.36	317.532	422.6	293	43239.36	835.923	523.4	329	95273.60	1842.291	624.2
218	16742.04	323.738	424.4	294	43902.16	848.929	525.2	330	96512.40	1866.285	626.0
219	17067.32	330.028	426.2	295	44580.84	862.057	527.0	331	97758.80	1890.346	627.8
220	17395.64	336.377	428.0	296	45269.40	875.367	528.8	332	99020.40	1914.742	629.6
221	17727.56	342.872	429.8	297	45964.04	888.799	530.6	333	100297.20	1939.401	631.4
222	18072.80	349.471	431.6	298	46669.32	902.437	532.4	334	101581.60	1964.267	633.2
223	18417.84	356.143	433.4	299	47382.20	916.222	534.2	335	102881.20	1989.398	635.0
224	18766.68	362.888	435.2	300	48104.20	930.183	536.0	336	104196.00	2014.822	636.8
225	19123.12	369.781	437.0	301	48833.80	944.291	537.8	337	105526.00	2040.540	638.6
226	19482.60	376.732	438.8	302	49570.34	958.533	539.6	338	106871.20	2066.532	640.4
227	19848.92	383.815	440.6	303	50316.56	972.903	541.4	339	108224.00	2092.710	642.2
228	20219.80	390.987	442.4	304	51072.76	987.386	543.2	340	109592.00	2119.163	644.0
229	20596.76	398.276	444.2	305	51838.08	1002.023	545.0	341	110967.60	2145.763	645.8
230	20978.28	405.654	446.0	306	52611.76	1017.343	546.8	342	112353.40	2172.637	647.6
231	21365.12	413.134	447.8	307	53395.32	1032.497	548.6	343	113749.20	2199.550	649.4
232	21757.28	420.717	449.6	308	54187.24	1047.810	550.4	344	115151.00	2227.199	651.2
233	22154.00	428.388	451.4	309	54989.04	1063.314	552.2	345	116561.40	2254.954	653.0
234	22556.32	436.207	453.2	310	55799.20	1078.980	554.0	346	118073.60	2283.171	654.8
235	22967.96	444.125	455.0	311	56612.40	1094.705	555.8	347	119592.80	2311.387	656.6
236	23382.92	452.152	456.8	312	57448.40	1110.871	557.6	348	121104.80	2340.044	658.4
237	23802.44	460.264	458.6	313	58284.40	1127.036	559.4	349	122620.40	2368.848	660.2
238	24229.36	468.523	460.4	314	59131.60	1143.496	561.2	350	124140.60	2397.799	662.0
239	24661.24	476.871	462.2	315	59989.40	1160.102	563.0	351	125661.20	2427.191	663.8
240	25100.52	485.365	464.0	316	60860.80	1176.856	564.8	352	127049.20	2456.730	665.6
241	25543.60	493.933	465.8	317	61742.40	1193.803	566.6	353	128599.60	2486.510	667.4
242	25994.28	502.647	467.6	318	62624.00	1210.950	568.4	354	130157.60	2516.837	669.2
243	26448.52	511.430	469.4	319	63528.40	1228.439	570.2	355	131720.80	2547.258	671.0
244	26912.36	520.400	471.2	320	64432.90	1245.927	572.0	356	133286.80	2577.819	672.8
245	27381.28	529.467	473.0	321	65332.90	1263.709	573.8	357	134854.40	2608.422	674.6
246	27855.52	538.638	474.8	322	66239.60	1281.618	575.6	358	136424.00	2639.088	676.4
247	28335.84	547.926	476.6	323	67144.40	1299.714	577.4	359	137995.20	2670.008	678.2
248	28823.76	557.360	478.4	324	68048.40	1317.937	579.2	360	139568.00	2701.093	680.0
249	29317.00	566.898	480.2	325	68951.40	1336.434	581.0	361	141142.80	2732.371	681.8
250	29817.84	576.583	482.0	326	69852.40	1354.971	582.8	362	142719.20	2763.854	683.6
251	30314.00	586.370	483.8	327	70752.40	1373.529	584.6	363	144296.80	2795.552	685.4
252	30817.76	596.305	485.6	328	71654.40	1392.181	586.4	364	145876.00	2827.371	687.2
253	31326.84	606.342	487.4	329	72558.40	1410.939	588.2	365	147457.20	2859.422	689.0
254	31838.04	616.556	489.2	330	73464.00	1429.700	590.0	366	149039.60	2891.699	690.8
255	32351.80	626.839	491.0	331	74372.00	1448.523	591.8	367	150624.00	2924.191	692.6
256	32867.40	637.292	492.8	332	75282.00	1467.400	593.6	368	152210.40	2956.894	694.4
257	33385.36	647.838	494.6	333	76194.00	1486.333	595.4	369	153798.40	2989.819	696.2
258	33905.40	658.601	496.4	334	77108.00	1491.203	597.2	370	155388.00	3022.971	698.0
259	34428.76	669.417	498.2	335	78024.00	1506.058	599.0	371	156979.20	3056.366	699.8
260	34954.00	680.273	500.0	336	78942.00	1520.932	600.8	372	158572.00	3089.994	701.6
261	35481.80	691.270	501.8	337	79862.00	1535.823	602.6	373	160166.40	3123.854	703.4
262	36012.00	702.403	503.6	338	80784.00	1550.730	604.4	374	161762.40	3157.941	705.2
263	36544.20	714.152	505.4	339	81708.00	1565.652	606.2				

Temp. °F	Pounds per sq. in.
148.782	357.8
152.221	359.6
155.719	361.4
159.275	363.2
162.890	365.0
166.560	366.8
170.286	368.6
174.067	370.4
177.897	372.2
181.678	374.0
185.402	375.8
189.171	377.6
192.886	379.4
196.548	381.2
200.258	383.0
203.916	384.8
207.523	386.6
211.178	388.4
214.782	390.2
218.335	392.0
221.938	393.8
225.491	395.6
229.094	397.4
232.647	399.2
236.250	401.0
239.803	402.8
243.406	404.6

CRC Handbook of Chemistry and Physics

A Ready-Reference Book of Chemical and Physical Data

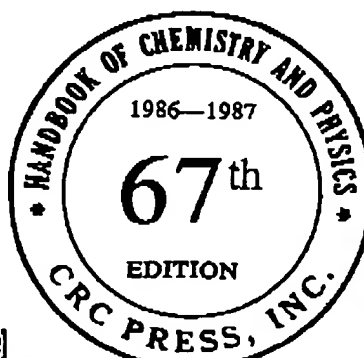


Table 4.7. Enthalpies of fusion and vaporization at the transition temperature, $\Delta H_m^\circ/\text{kJ mol}^{-1}$

	T_f/K	Fusion	T_b/K	Vaporization
<i>Elements</i>				
Hc	3.5	0.021	4.22	0.084
Ar	83.81	1.188	87.29	6.51
Xe	161	2.30	165	12.6
H ₂	13.96	0.117	20.38	0.916
N ₂	63.15	0.719	77.35	5.586
O ₂	54.36	0.444	90.18	6.820
F ₂	53.6	0.26	85.0	3.16
Cl ₂	172.1	6.41	239.1	20.41
Br ₂	265.9	10.57	332.4	29.45
I ₂	386.8	15.52	458.4	41.80
Hg ₂	234.3	2.292	629.7	59.30
Na	371.0	2.601	1156	98.01
Ag	1234	11.30	2436	250.6
<i>Inorganic compounds</i>				
H ₂ O	273.15	6.008	373.15	40.656 44.016 at \bar{f}

	T_f/K	Fusion	T_b/K	Vaporization
<i>Inorganic Compounds</i>				
H ₂ S	187.6	2.377	212.8	18.67
NH ₃	195.4	5.652	239.7	23.35
CO ₂	217.0	8.33	194.6	25.23 (s)
CCl ₄	250.3	2.47	349.9	30.00
CS ₂	161.2	4.39	319.4	26.74
H ₂ SO ₄	283.5	2.56		
<i>Organic compounds</i>				
CH ₄	90.68	0.941	111.7	8.18
C ₂ H ₆	89.85	2.86	184.6	14.7
C ₃ H ₈	278.6	10.59	353.2	30.8
CH ₃ OH	175.2	3.16	337.2	35.27
C ₂ H ₅ OH	156	4.60	352	37.99 at \bar{f} 43.5

Data: AIP.

Library of Congress Cataloging in Publication Data
 Atkins, P. W. (Peter William), 1940–
 Physical chemistry.
 Includes bibliographies and index.
 I. Chemistry, Physical and theoretical. I. Tide.
 QD453.2.A88 1985 541.3 85-7048
 ISBN 0-7167-1749-2

Copyright © 1978, 1982, 1986 by P. W. Atkins

Estimate of the Vapor Pressure of Water at 2500° C**I. Assumptions and Boundary Conditions.**

$$\Delta H_{\text{vap}}(\text{H}_2\text{O}) = 44.016 \text{ kJ mol}^{-1}$$

$\Delta H_{\text{vap}}(\text{H}_2\text{O})$ is constant as a function of temperature

$$P_{\text{vap}}(\text{H}_2\text{O}, 374^\circ \text{C}) = 1.65 \times 10^5 \text{ Torr} = 217 \text{ Atm}$$

$$T_1 = 374^\circ \text{C}$$

$$T_2 = 2500^\circ \text{C}$$

II. Estimate of $P_{\text{vap}}(\text{H}_2\text{O})$ at 2500 ° C using the Clausius-Clapeyron Relationship.

$$\ln \left(\frac{P_{\text{vap}}^{T1}}{P_{\text{vap}}^{T2}} \right) = \left(\frac{\Delta H_{\text{vap}}}{R} \right) \times \left(\frac{1}{T_2} - \frac{1}{T_1} \right)$$

$$\ln \left(\frac{P_{\text{vap}}^{T1}}{P_{\text{vap}}^{T2}} \right) = \left(\frac{(44.016 \text{ kJ}) \times \left(\frac{1000 \text{ J}}{1 \text{ KJ}} \right)}{8.3145 \text{ JK}^{-1}} \right) \times \left(\frac{1}{(2500 + 273) \text{ K}} - \frac{1}{(374 + 273) \text{ K}} \right)$$

$$\ln \left(\frac{P_{\text{vap}}^{T1}}{P_{\text{vap}}^{T2}} \right) = -6.28$$

$$P_{\text{vap}}^{T2} = \frac{P_{\text{vap}}^{T1}}{\exp(-6.28)} = \frac{217 \text{ Atm}}{0.00187} = 1.16 \times 10^5 \text{ Atm}$$